The Excavation of the 34th Street Station for the No.7 Line Extension and Grand Central Terminal Rock Caverns beneath New York

Peter Chamley Arup







Introduction

Two recent Rock Cavern Case Studies from New York will be discussed

> No. 7 Line Project (34th Street Station) East Side Access Project (Grand Central Station)

The presentation will focus on the site investigation, design and construction of the caverns on these projects

Geological Interpretation

Empirical / Numerical Design

Construction observations (movement, vibration etc)

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New Jersey

Brooklyn

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lan





Long Island

Manhattan Projects





No. 7 Line Project Overview

- 1st Design / Build Underground Project in NYC
- 1st Cavern excavated in NYC in 40 years – cavern complete on time
- 6+ months ahead of schedule (after 18 months)

Arup scope:

- Initial support design for station caverns and 26th Street TBM Launch cavern
- Site Presence, providing technical support and redesign work as required during construction









Owner: New York City Transit



New York City Transit Capital Construction

Contractor: S3II Tunnel Constructors



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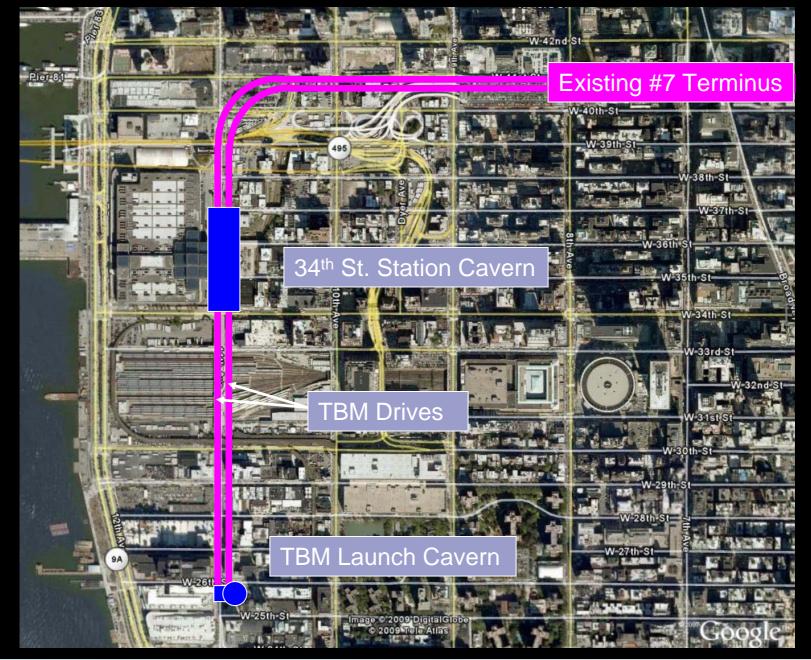
Owner's Engineer: Parsons Brinkerhoff

Construction Manager: Hill Intl/Liro/Lemley/HDR

Contractor's Designer: Arup

• Subconsultants: GZA, Snee Geoconsult







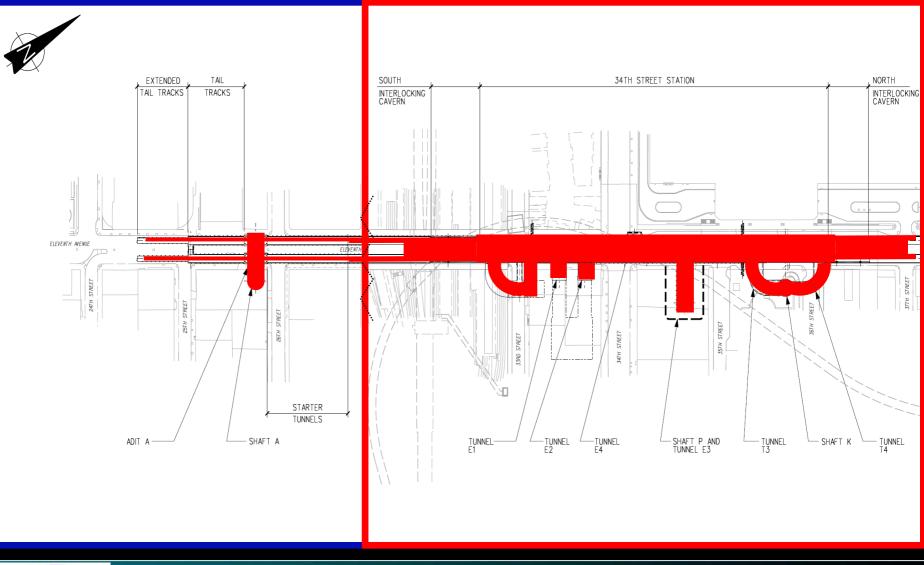






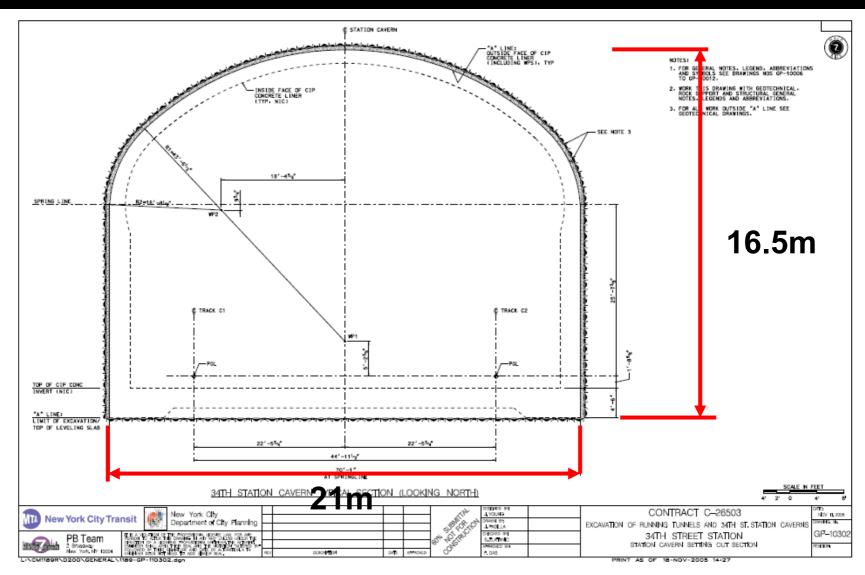


Anticipated Construction Sequence



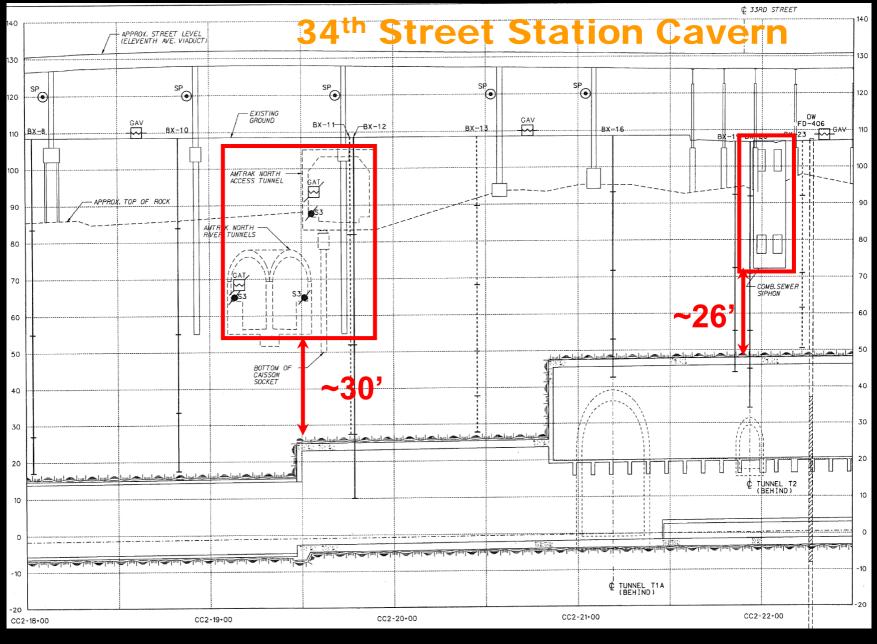


34th Street Cavern

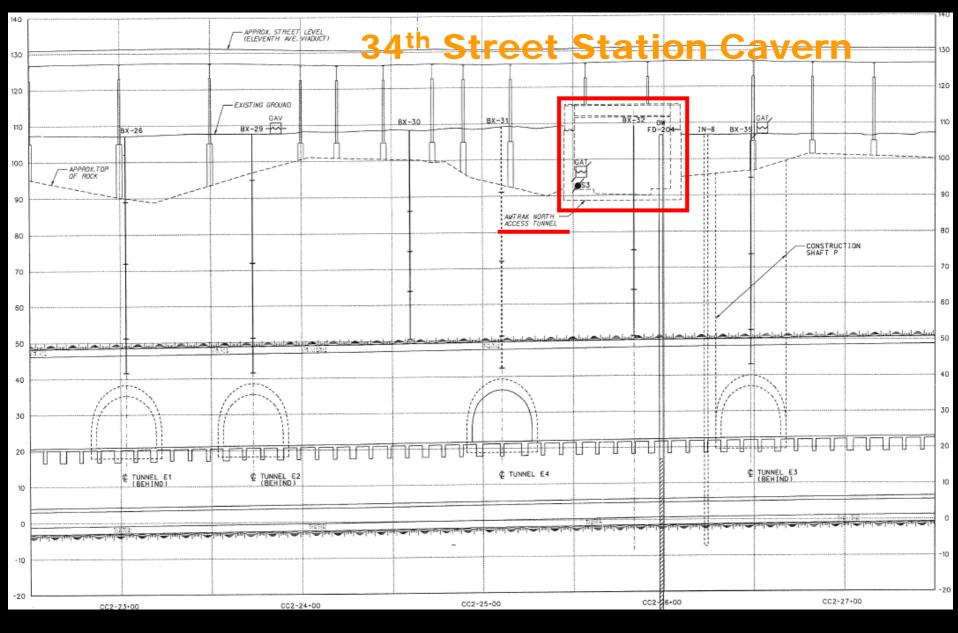




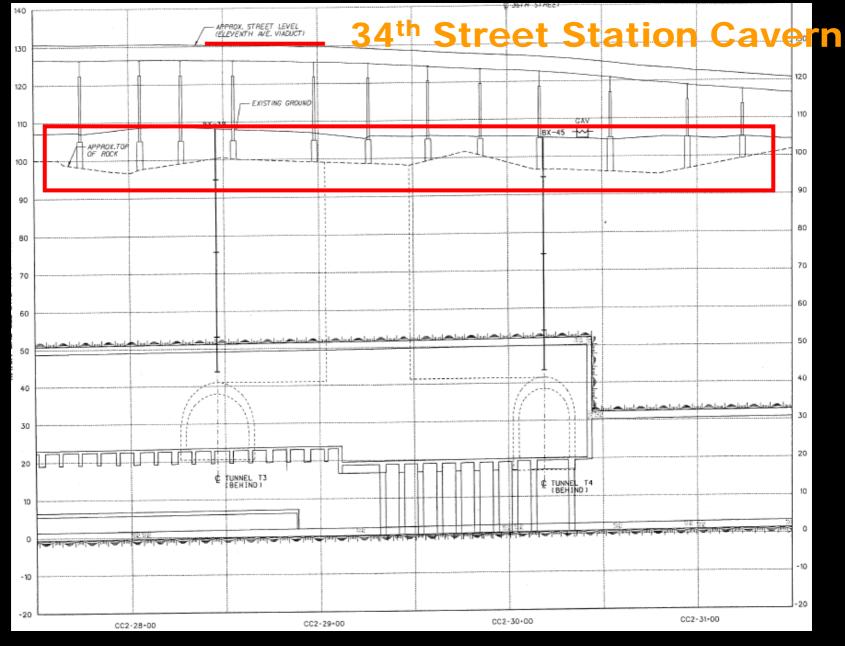










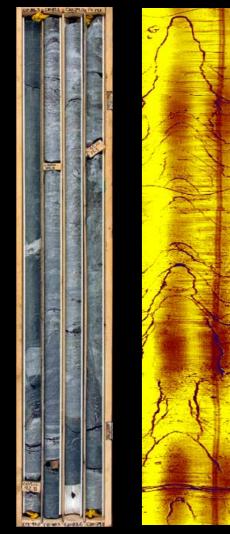


Sources of Information

Geotechnical Baseline Report

Geotechnical Data Report

- Subsurface Investigation
 - Soil and rock core logging, oriented core
 - Acoustic Televiewer corehole logging
 - Observation wells
 - Hydraulic fracturing tests
 - Rock core photographs
 - Laboratory testing of rock core
 - Geologic mapping



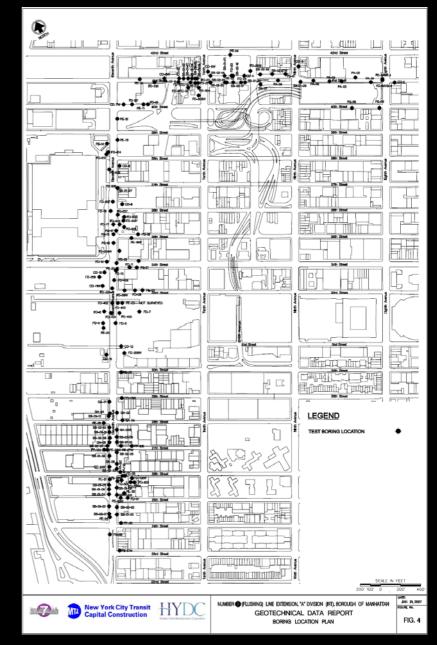
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 Information from TBM and Drill-and-Blast tunneling projects in NYC (historic, current i.e. THE Project)



Subsurface Investigation

- 164 geotechnical borings, 5 oriented, several phases
- 22 observation wells
- 228 packer tests in 89 boreholes
- 60 acoustic/optical televiewer logs
- 7 hydraulic fracture tests in 2 boreholes
- Extensive laboratory testing
 - UCS, triaxial
 - Tensile strength
 - Elastic constants
 - Petrography etc.



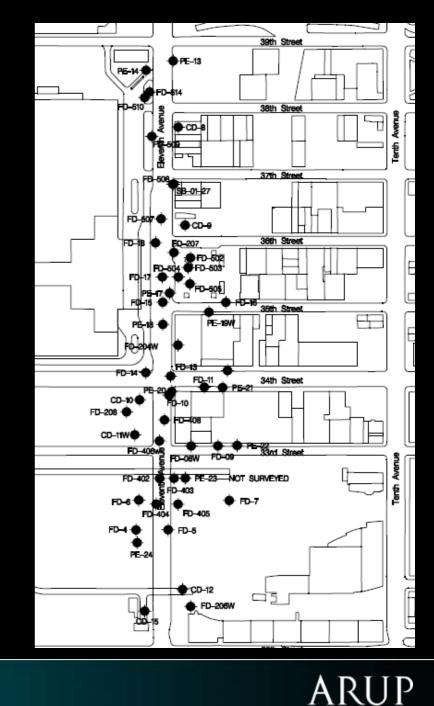
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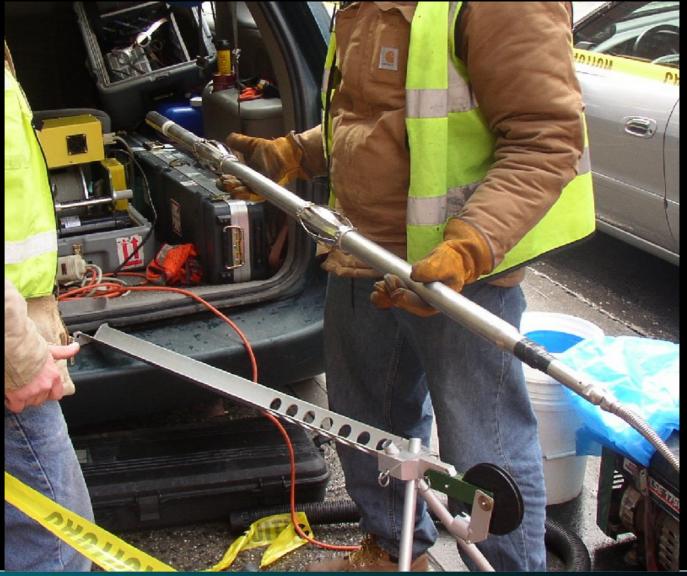
Subsurface Investigation 34th Street Cavern

- 49 existing boreholes
- 26 additional borings planned by Arup/GZA
- Surface mapping of outcrops





Acoustic televiewer

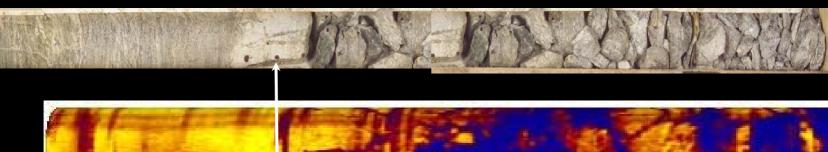


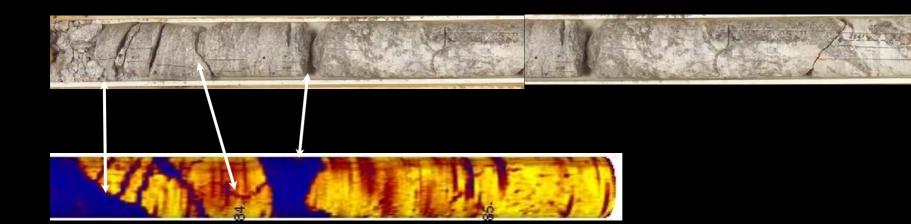




Correlation of ATV and Core









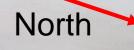








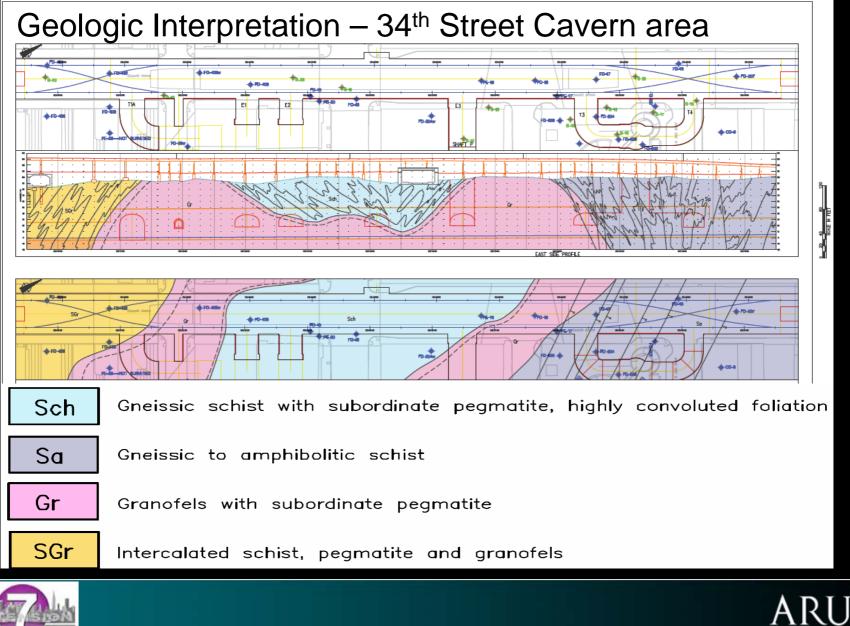
Decomposed foliation jointing







Geologic Interpretation



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Geological Interpretation

- Geotechnical interpretations on plan / section
- Three rock classes:
 - A Q > 3.5; RMR > 55
 - B Q range 1.5 to 3.5; RMR range 45 to 55
 - C Q < 1.5; RMR < 45
- Particular concern with character of rock mass in north end of 34th Street Cavern
- Contact zones



Schist / Granite Contact





Contact at Site A

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Contact at 34th Street Cavern



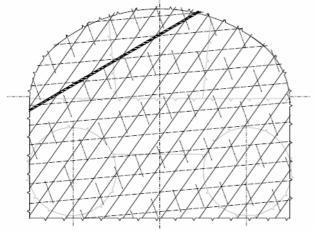
Design Philosophy

- Shallow Cavern, in hard competent rock
- Cavern / Tunnel Stability is controlled by structural discontinuities within a competent rock (i.e. problem is not one of stress, but stabilizing wedges)
- Provide support to ensure interlocking of these blocks and limit block movement along joints

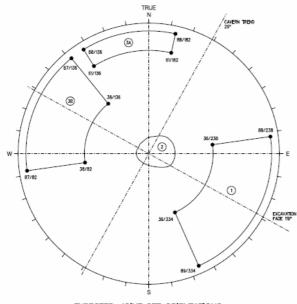




Rock Mass Classes



ROCK MASS CLASS TYPE B



EXPECTED JOINT SET ORIENTATIONS LOWER HEMISPHERE EQUAL ANGLE

TABLE 1: EXPECTED ROCK TYPE AND STRENGTH TO BE VERIFIED DURING CONSTRUCTION BY PARAMETER EXPECTED RANGE DISCUSSION ROCK MASS DESCRIPTION AS CHARACTERIZED BY TERZAGH OBSERVATION MASSIVE TO MODERATELY JOINTED SCHSTI WED DARK GRAY TO BLACK PRINCIPALLY COMPOSED OF BIOTTE, QUARTZ, PLALOCLASE FELOSPAR, SOME MISTINEIROS. GRANTLEGENORTES, FINK TO GRAY 1-10 GRAND, COMPOSED OF QUARTZ, K-SPAR, MUSCOVITE, MINERALOGY OBSERVATION SOME MINERAL ALIGNMENT. RESULT OF THE UNAXIAL COMPRESSION STRENGTH TEST GIVES THE RANGE FROM 5,800 TO 39,000 (PSI), AVERAGE 21,000 (PSI) GEOLOGICAL HANNER NORE THAN 1 FIRM BLOW TO BREAK SCHIST: 5,700 - 13,900 (PSI) GRANTE: 9,700 - 31,300 (PSI) ROCK STRENGTH SLIDHT RUST DISCOLORATION ON SURFACES, SOME OR ALL MATERIAL WAY BE SOMEWHAT WEAKER EXTERNALLY THAN IN ITS FRESH CONDITION. UNIVERTHERED TO SLICHTLY WEATHERED (W1 - W2) WEATHERING GRADE OBSERVATION

TABLE 2: STRUCTURAL GEOLOGY				
PARAMETER	DISCUSSION TO BE VERIFIED DURING EXPECTED RA		EXPECTED RANGE	
JOINT SYSTEM	THREE TO FOUR JOINT SETS	COMPASS MEASUREMENT		
TYPICAL BLOCK SIZE	EQUIDIMENSIONAL OR CUBICAL BLOCK	JOINT VOLUME	2 (CUFT.) TO > 100 (CU.FT.)	
FAULTS/SHEAR ZONES	OBSERVED SHEAR PLAYES TYPEALLY OCCURING AT SCHET GRANDFELS CONTACT, CONTAN CLAY OR DISINTEGRATED ROOK RETWEEN ROOK SURFACES, WITH A THORNESS OF ALTERATION PRODUCTS NOT TO EXCEED 5 INCHES	OBSERVATION	1 PER FACE	
IN SITU STRESS	NO POPPING ROCK EXPECTED, POPPING ROCK MATERIAL INDICATES HIGHER IN SITU STRESS THAN ANTIOPATED	OBSERVATION	1 - 2	

TABLE 3: JOINT INFORMATION					
EXPECTED JOINT TYPES	SET 1	SET 2	SET 3	TO BE VERIFIED DURING CONSTRUCTION BY	
	FOLIATION SET	SUBHORIZONTAL	CROSS FOLIATION		
AVERAGE ORENTATION (DIP ANGLE/DIRECTION)	54 / 287	12 / 270	34/77 / 156, 38:60 /107	COMPASS MEASUREMENT	
APERTURE	CLOSED	0.5 - 1.0 N (OPEN)	CLOSED MEASURING TAPE		
SPACING	FROM 2 FT TO 5 FT	FROM 2 FT TO 5 FT	FROM 2 FT TO 5 FT MEASURING TAVE, SCANLINE		
PERSISTENCE	HIGH PERSISTENCE	HIGH PERSISTENCE	LOW PERSISTENCE (GENERALLY LESS THAN 6 FT)	MEASURING TAPE	
ROUGHNESS	SMOOTH UNDULATING TO SLICKENSIDED (AVERAGE Jr - 2)	SMOOTH UNDULATING TO SLICKENSIDED (AVERAGE Jr - 2)	SMOOTH UNDULATING TO SUCKENSIDED JRC TABLE / LINEAR PROFILING / PROFILE (AVERAGE Jr - 2)		
ALTERATION	UNALTERED TO NON-SOFTENING MINERAL COATING (AVERAGE Jg - 2)	UNALTERED TO NON-SOFTEMING MINERAL COATING (AVERAGE JD - 2)	UNALTERED TO NON-SOFTENING WHERAL COATING (AVERAGE to - 2) Jo (0 SYSTEM)		

TABLE 4: GROUNDWATER CONDITIONS				
PARAMETER	TO BE VERIFIED DURING CONSTRUCTION BY	EXPECTED RANGE		
GENERAL CONDITIONS	OBSERVATION	DRY OR WINDR Inflow (K 5 L win), Dripping discontinuities, Also short term wodenate inflow from set 2 joints		
EXPECTED INFLOW	OBSERVATION	5 - 20 L / WN / 10 FT OF DRIFT		

TABLE 5: ROCK MASS CHARACTERIZATION				
SYSTEM	DISCUSSION	TO BE VERIFIED DURING CONSTRUCTION BY	EXPECTED RANGE	
TYPICAL ROCK CORE QUALITY (RQD)	GENERAL ROD VALUES RECORDED FROM BOREHOLE DATA IS IN THE RANCE FROM 80 TO 100, OBCRETE ZONES OF ROD VALUES OF 50 MAY BE ENCOUNTERED OVER LIMITED DISTANCE/EXTENT.	JOINT VOLUME ESTIMATION ON UNIT VOLUME OF ROCK	80 - 100 (2)	
GSI		GEOLOGICAL MAPPING	55 - 70	
Q,	Q' = RQD / Jn x Jr x Jo	GEOLOGICAL MAPPING	5 - 20 (AVERAGE 10)	
RMR		GEOLOGICAL MAPPING	37 - 72 (AVERAGE 58)	
TERZAGH	•	GEOLOGICAL MAPPING	MODERATELY JONTED - MODERATELY BLOCKY OR SEAWY	
STANDUP TINE		OBSERVATION	10 HOURS - 2 YEARS (AVERAGE 1 MONTH)	

8' 4' 0 8' 16'





Rock Mass Classification – Q System

• Joint number (Jn)

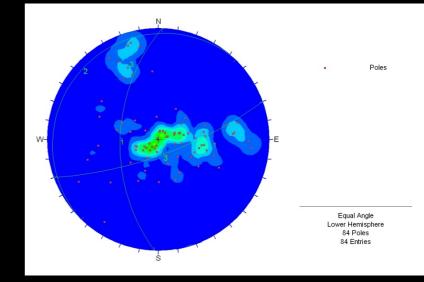
ATV data along cavern alignment;

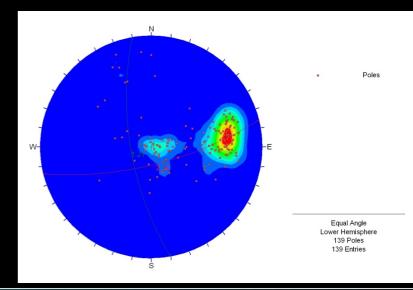
Consistent joint orientations (3 sets) for Jn=9 rating

(exception is tail/starter tunnels and Shaft/Adit A where Jn=6)

• RQD, Jr, Ja

Obtained directly from boring logs, verified by field logging and additional boreholes

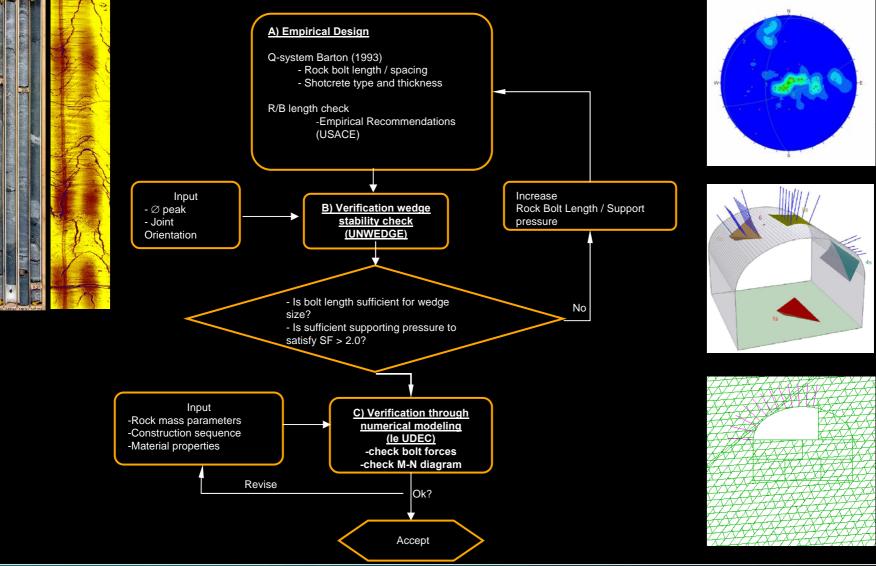




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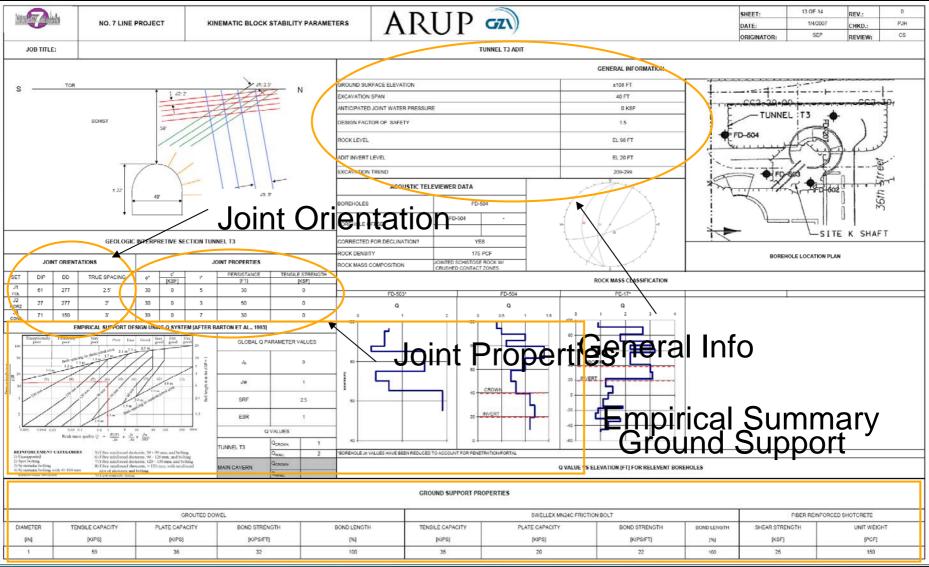


Simplified Cavern Design Methodology





Summary Sheet





Key Block Analysis

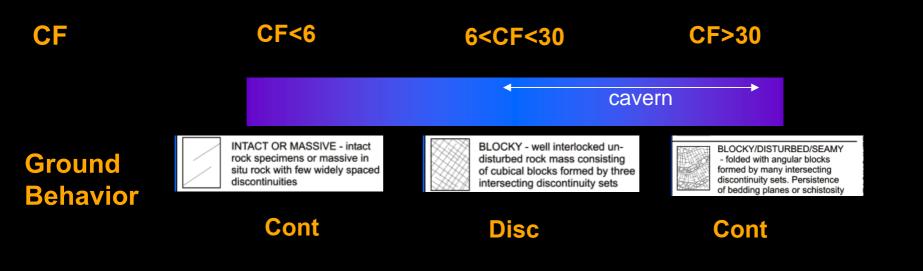
- Use of UNWEDGE software at sections through cavern and adits where ATV data was available (17+ sections completed to date)
- Support input was that determined by empirical method (Q, USACOE)
- Accounted for overbreak





Numerical Model Verification

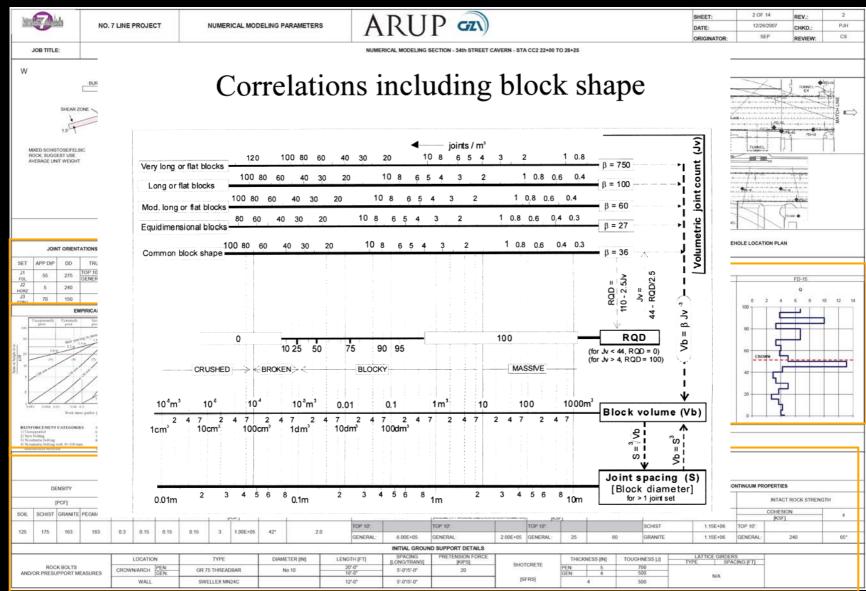
- UDEC for discontinuum, FLAC for continuum
- Distinguished by ratio of cavern span/estimated block diameter (continuity factor); i.e. no. of blocks occurring along cavern roof (Palmstrom 2005,2008)



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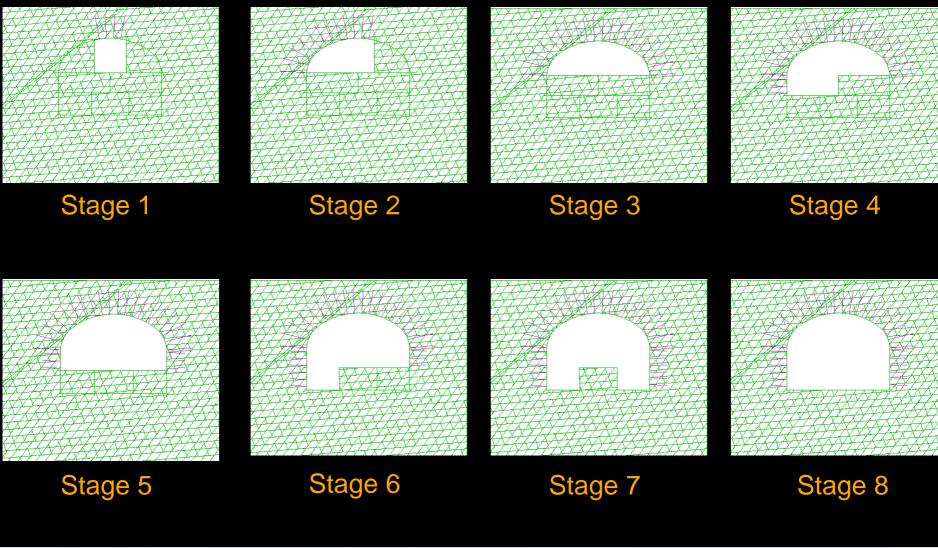
UDEC Input Properties





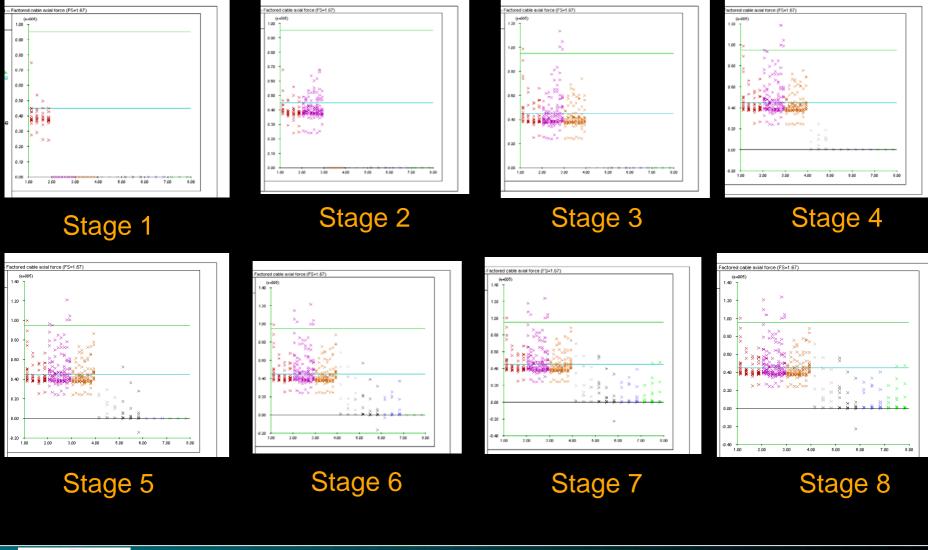


Typical UDEC Modeling Construction Sequence



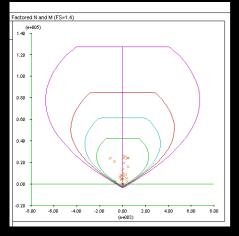


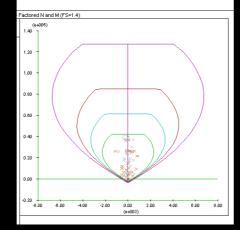
UDEC Results - Type B Support Rock Bolts



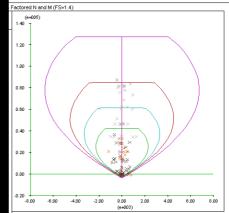


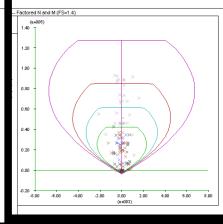
UDEC Results - Type B Support Shotcrete



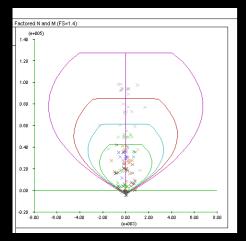


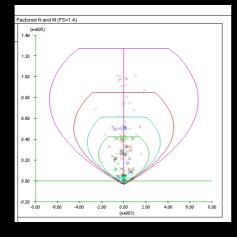
Stage 2

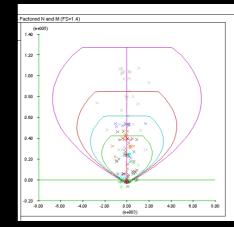




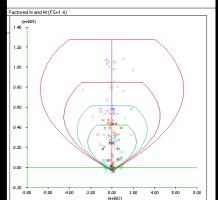
Stage 1







Stage 3



Stage 4

Stage 5

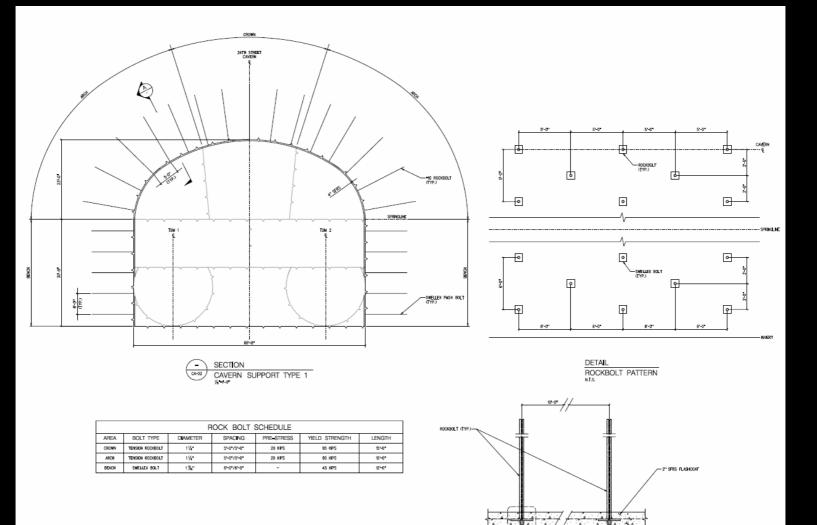
Stage 6

Stage 7

Stage 8



Support Type 1



14.

A

. N.T.S.

SECTION

- NTRACOS OF FINAL LINING AND WATERPROOFING 8' 4' 0

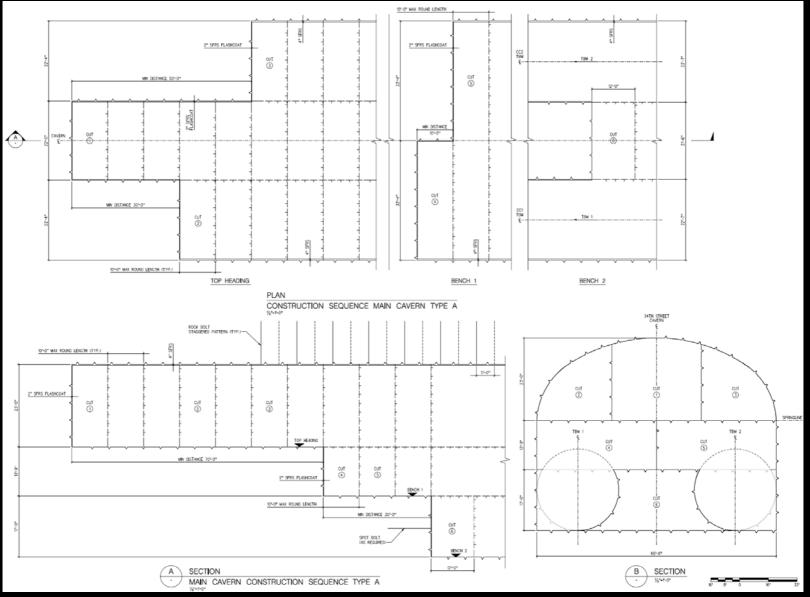
SEE DETAL DWG. NO7-5A-DT-01-



16' 8



Proposed Construction Sequence



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Support Types

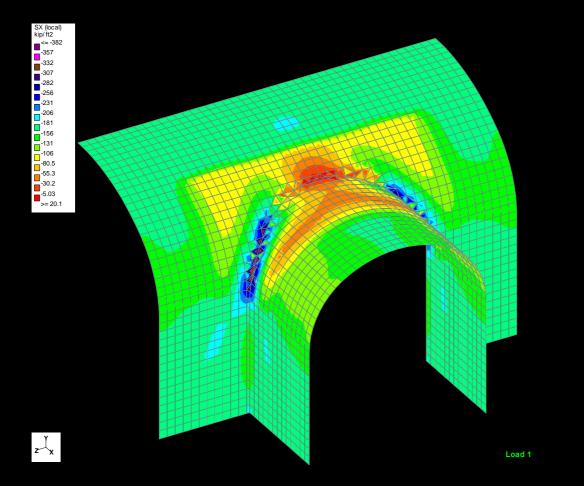
Support Class	Dywidag Bolt Length	Pattern (Crown & Arch)	Shotcrete (inches)
1	15	5 x 5	4
2	15	5 x 5	6
3	18	5 x 5	6

Support Class	Swellex Bolt Length	Pattern (Bench)	Shotcrete (inches)
1	12	6 x 6	4
2	12	6 x 6	6
3	12	6 x 6	6





Shotcrete Junction Analysis – Axial Stress

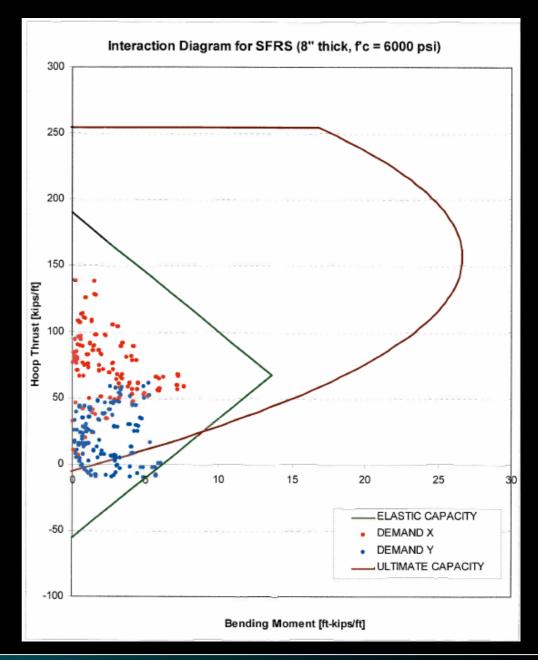






Typical interaction diagram at junction

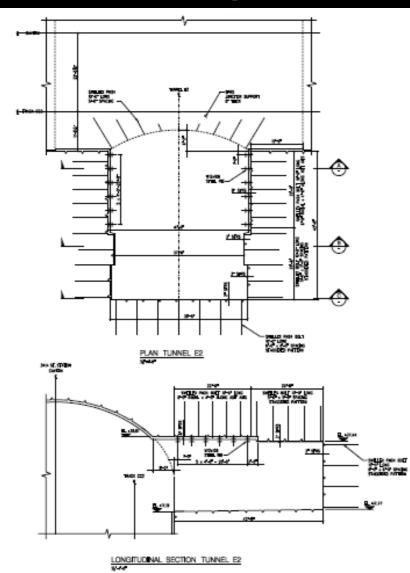
- Points represent forces in FE plate elements in both directions (3D)
- All points within elastic capacity curve $\sqrt{}$ ok

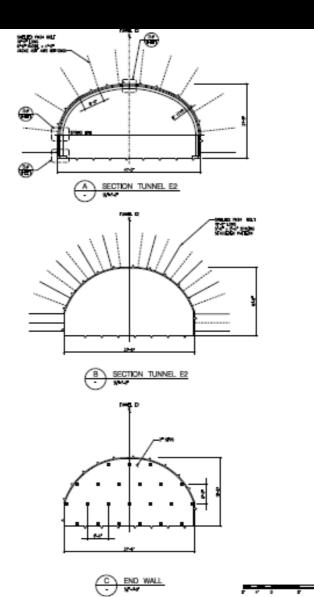


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Junction Design







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Construction Photos



Shaft A –

TBM Assembly Cavern

Shaft P – 34th St. Station Cavern





TBM Assembly Chamber / Starter Tunnels



















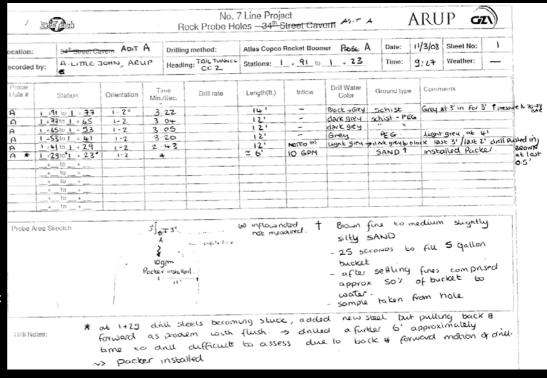
Bolt testing & probing

3% of all installed bolts tested

Tests to 1.3P for Dywidag bars to verify the design capacity achieved

Swellex tested to 74kips failure deamed as 12" displacement.

Pobing always maintained a minimum of 30ft (9.1m) ahead of tunnel face at all times, to verify cover and competent ground as construction advanced





34th St Station Cavern Break-in







Cavern Top Heading Excavation







Cavern / Ancillary Tunnel Junction







Staggered Headings













Ramp Down to Start Benching







Complex Geometries















Benching













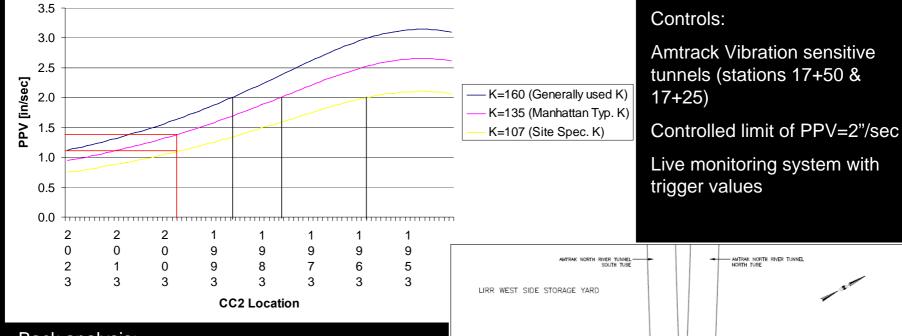
Fully Developed Cavern Excavation







Blast Vibration Monitoring & Analysis

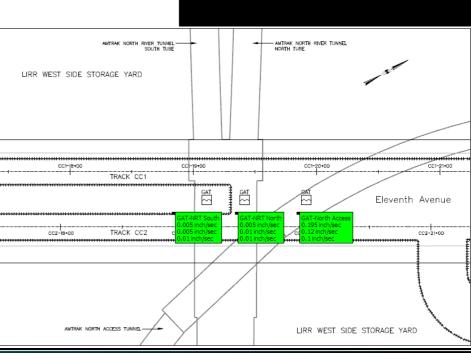


Back analysis:

From Monitoring data established site specific K (ground constant value) of 107.

Compared data with respect to distance from source and Maximum Instaneous Charge (MIC) for SS K value and referenced data in Schist.

Used to predict vibrations and control shot lengths during construction using the lifetime monitoring (right).



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Instrumentation data - settlements

- All movements were less than predicted
- Typically around 25% of that predicted by UDEC

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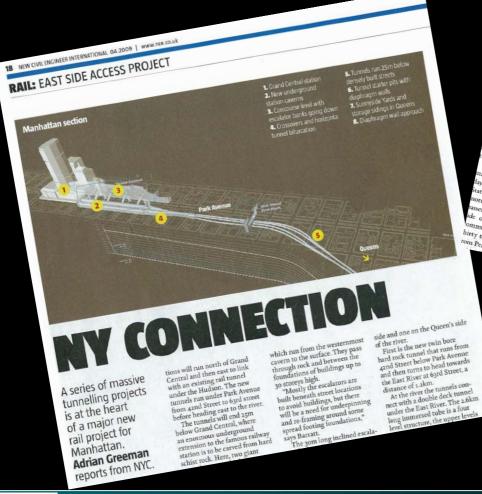
- Why ? -
 - Joint Persistence
 - Joint Waviness
 - Joint Condition



Grand Central Caverns – East Side Access

MTA Contract CM-019 Arup Scope

Initial Ground Support Design







East Side Access – Grand Central Terminal Caverns







Grand Central Terminal







East Side Access - Grand Central Caverns







Grand Central Caverns - Project Team

- Owner: Long Island Rail Road
- Owner's Engineer: GEC (Parsons Brinkerhoff/ STV /PTG)
- Construction Manager: URS/ Hatch Mott MacDonald
- Contractor: Dragados Judlau JV
- Contractor's Designer: Arup





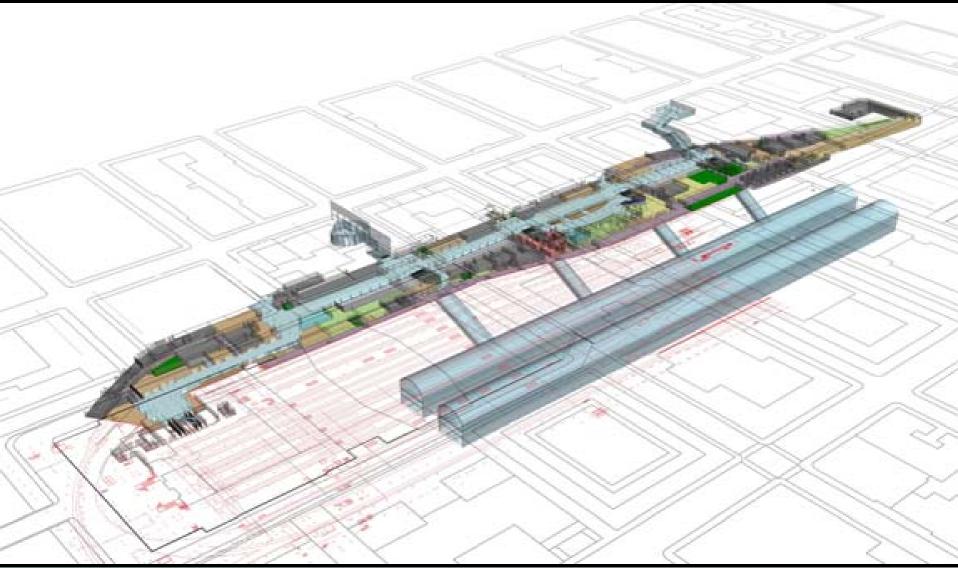
Grand Central Caverns







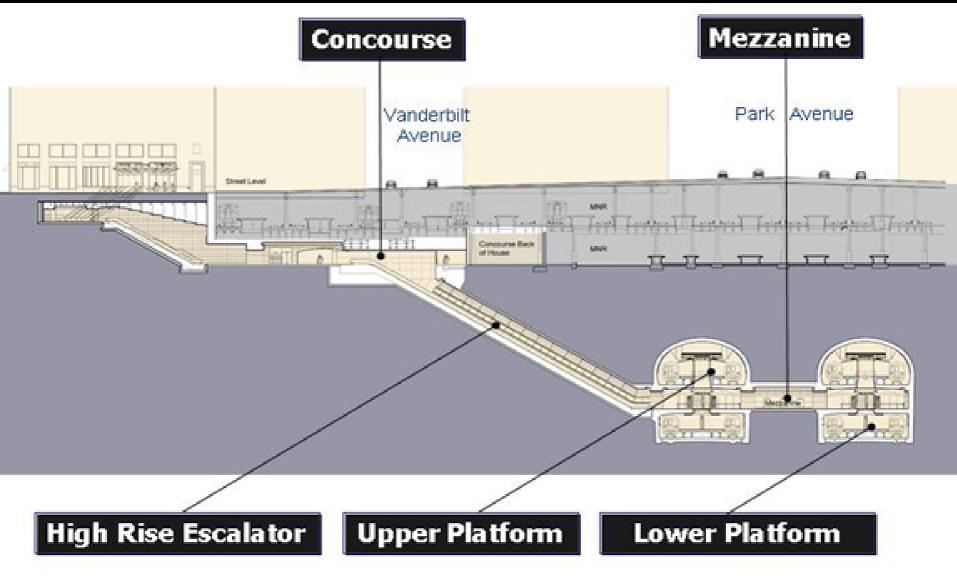
Grand Central Caverns





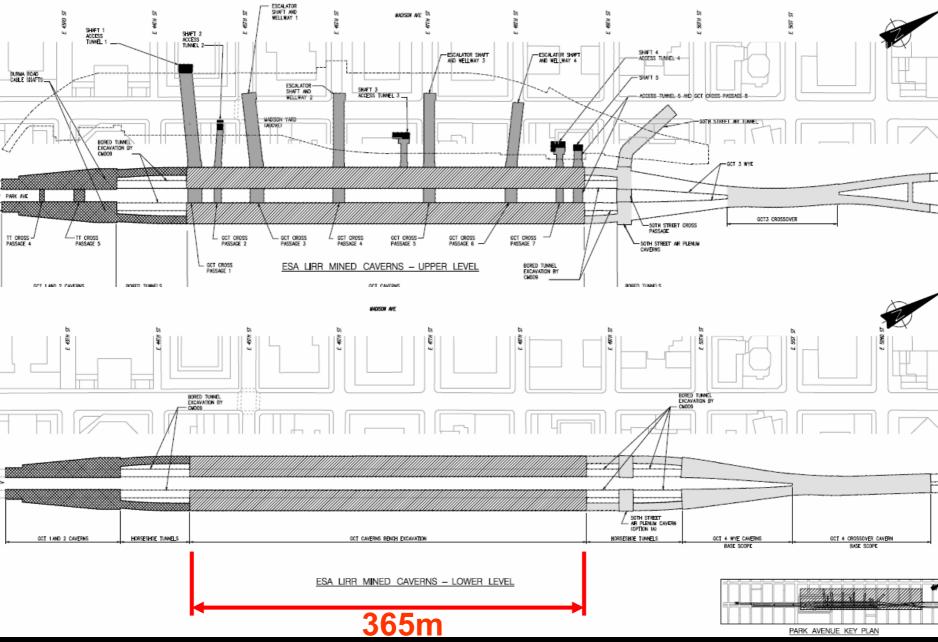


Grand Central Caverns



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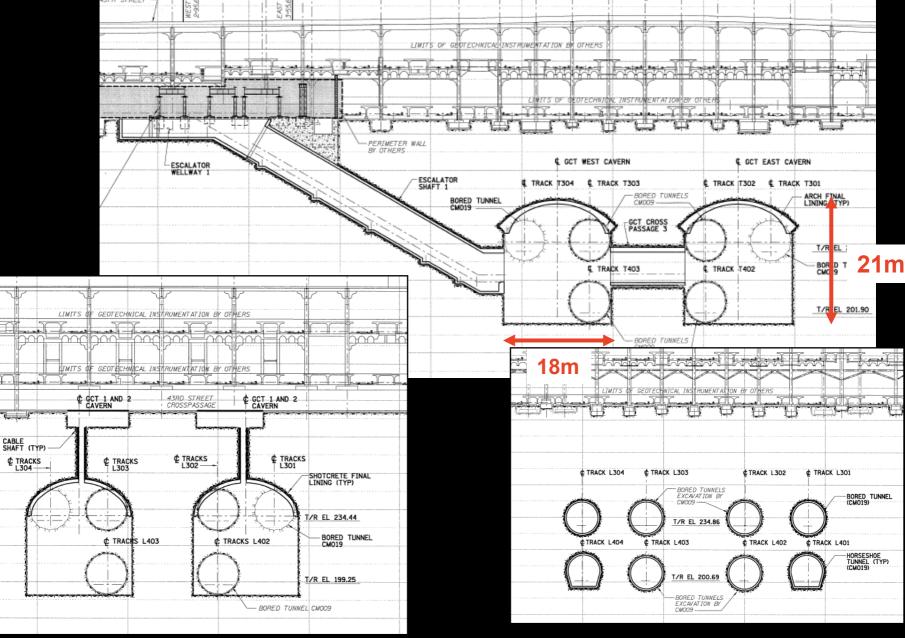








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PARK AVE

r BUTL

STREET GRADE 45TH STREET

Scope of Work – East Side Access Project

- Following completion and logging of the initial running tunnels, design of the cavern initial support.
- Initial work included geological mapping
- Design of Initial Ground Support
- Design completed, cavern construction has recently started.



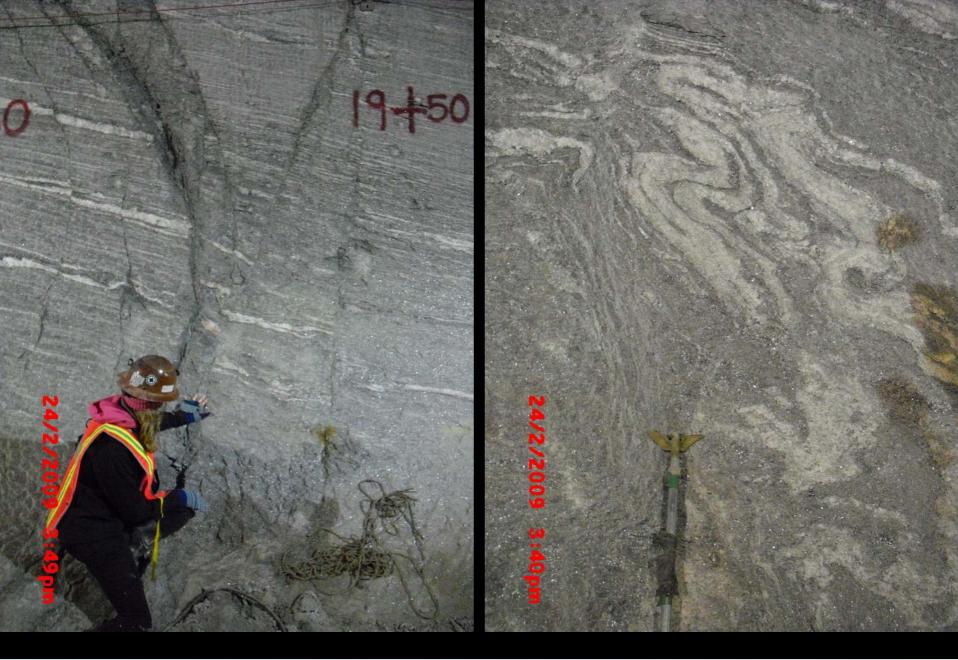
GCT – TBM Drive

1540

ARUF











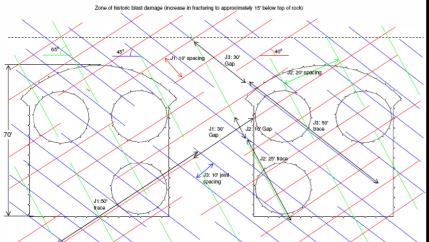
Rock Mass Zones

		Job	b No.			Sheet No.	Rev.				
ARUP					20	207975					
111		Mem			nber/Loc	ation					
Job Title	CM019 - Grand Central Caverns			Drg.	Drg. Ref.						
Calculation	Figure B.1 Geological Interpretation - Ground Type I, Package III, Central Cavern, Station 20+0	00 to 24+50.		Mad	de by	ACL		Date March 2009	Chd. _{PJH}		
A. Geological	Section looking North along the cavern axis			•	С	. Structural Geology					
Zone of historic blast damage (increase in fracturing to approximately 15' below top of rock)						Cavern Face (looking North)					
J1:50' Trace							Standard deviation ar 1 (Foliation) 40/ 40	S ad Variance refer to the +/- r 2 (Cross - Foliation) 60/ 65	ange from the mean value 3(conjugate to J1) 50/45		
			$\times X$			True/ Apparent Dip S.D.	20	20	35		
		\searrow	$\times \wedge \times$		D	ip Direction (S.D.)	270 (30)	150 (40)	90 (30)		
Referenced B	oreholes for no. of fractures per core run: MG115, MG204, MG118, MG203, MD11, MG54, MG122, MG120, MG202, M	D10			В	aseline Dip (GIR)	35	85	35		
	used for orientations: TBM Mapping T304 16+80 to 28+60 (24th July to 22nd August 2008) and TBM Mapping T30117-		8th July 2008)		В	laseline DD (GIR)	250	190	75		
	Zone Description (from GIR June 2008, Section 5.0 and Figures 3 sheets 1 - 4) I Geological Zone reference T402 18+50 to 31+00	D. Joint Properties Set No.	1 (Foliation)	2 (Cross-Foliation)		3 (Conjugate to J1)	G. Structures/ Shear	∠ones			
Dominant geo 50% of rock r	ology: Garnetiferous Schistose Gneiss and Gneiss nass moderately to widely spaced foliation fractures, 50% closely to moderately spaced nass widely spaced loints. So% closely to moderately spaced	Joint Trace (ft)	50' (Mean) 20' (Variance)	25' (Mean) 10' (Variance)	,	50' (Mean) 20' (Variance)					
Few infilled jo	rpically places of the second se	Joint Gap (ft)	30' (Mean) 15' (Variance)	10' (Mean) 5' (Variance)		30' (Mean) 15' (Variance)					
Joint set 2 - u near shear zo	prear by parane to characterize and rough reclaiming rough to very rough with occasional infill of sand and clay and surface staining with iron oxide, particularly nes and in areas of intense Pegmattle formation. esh, closed set, typically undulating and rough to very rough with no infill.	Joint Seperation (ft)	10' (Mean) 2.5' (Variance)	20' (Mean) 5' (Variance)		10' (Mean) 2.5' (Variance)					
RQD 7 5-90%	/ Q 1.5-10/ RMR 53-79	Friction Angle (°) øb	30-40 (35)	30-40(35)		40-50 (45)	Notes:				
	anticipated 5' below GCT track level/ Range of Coeff. of Permeability 10 ⁻⁵ to 10 ⁻⁷ cm/sec rater is currently pumped. The water level at the invert of GCT suburban level is EL 310, the water level at the East	Dilation Angle (°)øi	3-10 (5)	3-10 (5)		3-10 (5)	The rock properties in the blast damaged zone (15' below top of n currently being reviewed and revised rock properties may be prov final calculation submission.				
River is at EL	300.	Cohesion (lbf/ft ²)	0	0		0					
	nels (zones of anticipated weakness/shear zones and higher hydraulic conductivity in rock mass) from Viele 1874: stations where streams are anticipated to intersect with cavern, trending SE to NW East Cavern 18+00 to 19+00 and	Alteration (J _a)	1	1		1	4				
	+80; West Cavern 19+25 to 20+00.	Roughness (J,)	1.5	1.5		1.5					
		JRC Ave (Range)	10 - 12 (2-20)	14 - 16 (12-18)		12-14 (2-20)					

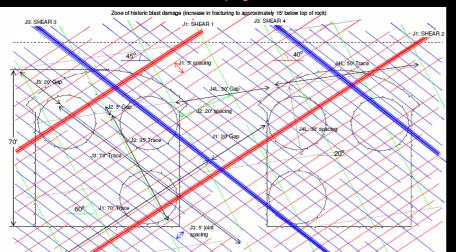
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Rock Mass Zones – Idealised Models

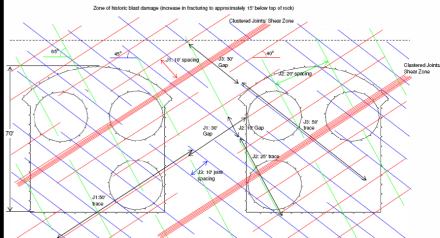


Type 1: Typical, 3 Joint sets J1 parallel to Foliation, J2 Sub-vertical set, J3 conjugate to J1

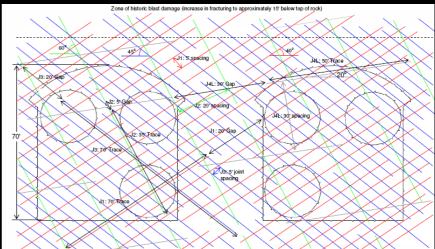


Type 3: Variation in spacing and persistence modeling presence of 2 shear zones on J1 and J3



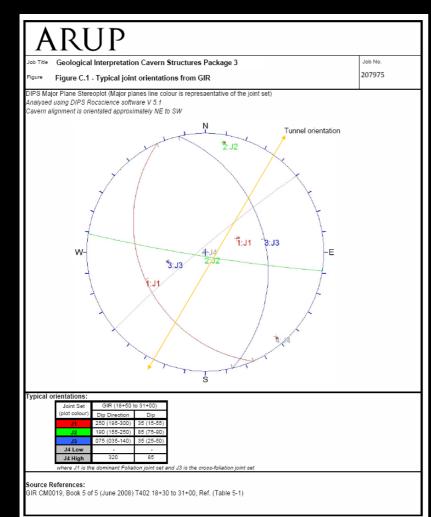


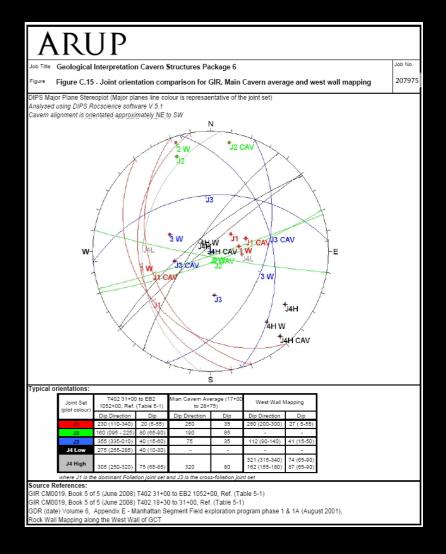
Type 2: Anticipated, as for type 1 with inclusion of zone of very closely jointed rock



Type 4: Worst case model, including a 4th Joint set, this is a modeled worst case condition NOT anticipated ARUP

Key Joint Sets

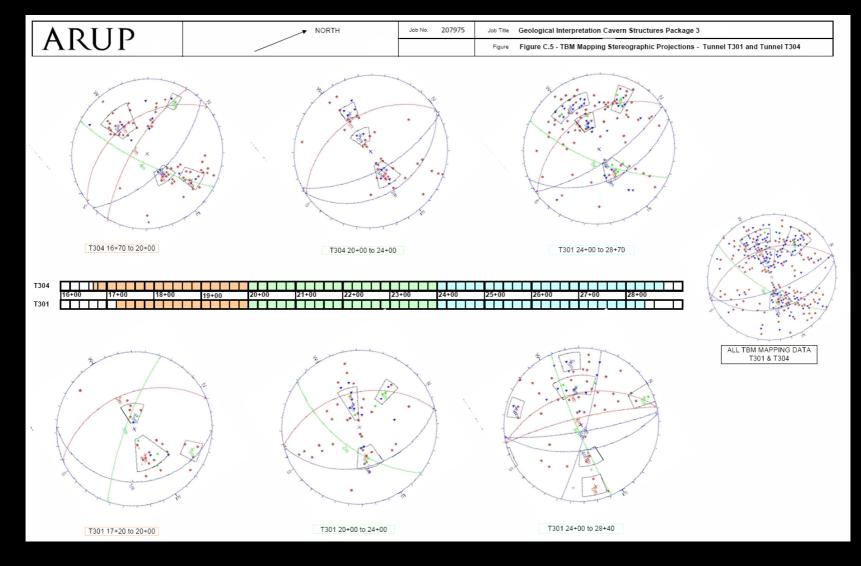








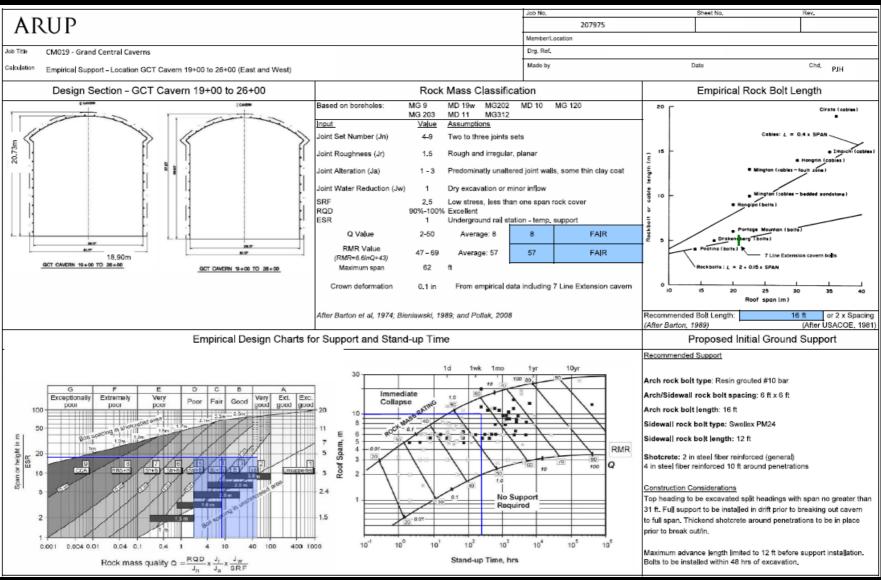
TBM Stereoplots with station T301







Emperical & Kinematic Assessment



ARUP



			Jab No.				Sheet No.		Rev.
ARUP			207975 9						
M			Member/Location						
Job Title CM019 - Grand Central Caverns			Drg. Ref.					Che	d.
Celculation Main Cavern STA 17+00 to 28+75 UNWEDGE Summary - Crown Critical Case (input & results) Rock Mass Type IV			Made by	SP		Date 03/02/2009			рн
Design Section model schematic including all loadings					UNWEDGE Input Prop	perties			
		20			General Project Conditions: Tunnel Axis Orientation: 029°, 0° plunge Unit Weight of Rock: 175 pcf Seismic Force: Not considered In-situ Stress: Using the measured in-situ stress values of about 2 vull only load to less conservative results, as such, they are not considered in the kinematic analysis. Joint Properties: Shear Strength Model: Mohr-Coulomb Ph: 35° (Joint Sets 1 & 4), 45° (Joint Sets 2 & 3) Tensile Strength: 0 ksf Cohesion: 0 ksf Water Pressure: 0 ksf Structure / Waviness: 0° (assumed planer, conservative) Wedges Scaled to: 35,70, 50 ft trace length (respectively)				
		15			Ground Support Pro	perties: Gr	ound Support Patter	<u>ı:</u>	
	Top - Al Wedges Scaled	Perspective - All Wedges Scaled *			Bond Strength: 32 kip Wall: Friction Bolts: Swelex Tensile Capacity: 45 J Plate Capacity: 20 kip Bond Strength: 8 kips Shear Strength: Not	#10 dps (60% GUTS) s (washer circumference s / ft 12: PM24 dps s / ft	-ft ong, 5-ft x 5-ft stagg	= 58 ksi)	
		Jo	int Orientatie						
		F		nt Set le Dip	1 (Foliation) 40	2 (Cross - Foliation) 80	3 (conjugate) 70	4 (Low) 20	4 (High) 70
				ie Dip Virection	270	150	70	320	305
		F	Baseline	Dip (GIR)	35	85	35	20	70
			Baseline	DD (GIR)	250	190	75	320	305

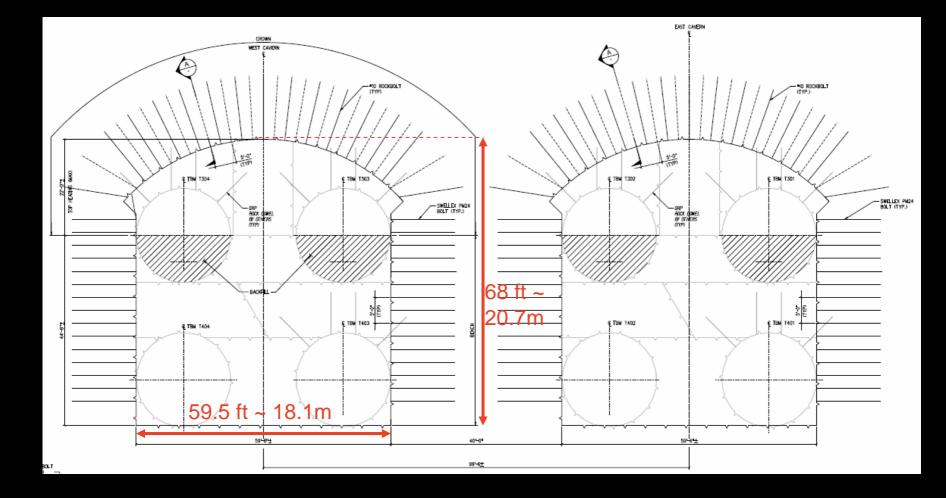
Wedge Scaling: Crown wedges scaled to approximately 2/3 maximum excavation height, or 40 feet.

Critical





Grand Central Caverns







Selection of Rock parameters

GDR/GBR baseline properties; used for continuum and discontinuum models

Property	Value	Notes
Rock Density (γ)	175 pcf	Derived from laboratory testing results presented in the GDR
Poisson's Ratio (v)	0.23	Derived from laboratory testing results presented in the GDR
Failure Envelope Range (σ_{3max})	12 ksf	Calculated at cavern crown level from in situ stress and surcharge loads
Intact Rock Cohesion (ci)	210 ksf	Output from RocLab based on input of above parameters; within accepted range for Manhattan Schist
Intact Rock Friction Angle (¢i)	55°	Output from RocLab based on input of above parameters; within accepted range for Manhattan Schist
Young's Modulus (Ei)	8.65E+05 ksf	Derived from laboratory testing results presented in the GDR
Tensile Strength (σt)	150 ksf	Calculated by tension cutoff: c/tan ø
In situ Stress Ratio (K)	2	From hydrofracture testing in Manhattan from various tunnelling projects

	Va	lue					
Property	Ground Type D Disturbed (Blasting) Zone		Notes				
Unconfined Compressive Strength (UCS)	1008 ksf		Derived from laboratory testing results presented in the GDR				
Geological Strength Index (GSI)	5	0	Based on rock core photographs and logs; a qualitative assessment of the rock mass as "very blocky" with "fair" to "good" surface quality condition; as per Hoek et al. 1995				
Poisson's Ratio (v)	0.2	25	Derived from laboratory testing results presented in the GDR				
Disturbance Factor (D)	0.0 0.8		Rock mass considered undisturbed for general analysis but severely impacted for 5 ft zone beyond drill and blast excavation perimeter; as per Hoek et al., 2002				
Failure Envelope Range (o _{3max})	12 ksf		Calculated at cavern crown level from in situ stress and surcharge loads				
Deformation Modulus (Em)	2.2E+05 ksf	1.1E+05 ksf	Output from rock mass modulus reduction, values verified using RocLab				
Rock Mass Cohesion (c)	10 ksf	7.5 ksf	Output from RocLab based on input of above parameters; within accepted range for Manhattan Schist				
Rock Mass Friction Angle (55 50		Output from RocLab based on input of above parameters; within accepted range for Manhattan Schist				
In situ Stress Ratio (K)	2.	0	From hydrofracture testing in Manhattan for various tunneling projects				

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JP

Table 2: Continuum Input Parameters for Ground Type D



		lah Na			Sheet No.		8	
ARUP	Job No. 207975			ondet NO.	Rev.			
ARUP								
		Member/Location						
Job Title CM019 - Grand Central Caverns		Drg. Ref.				Chd.		
Calculation UDEC Summary (input & results) Rock Mass Type II (South and M	Made by PJH Date PJH							
DESIGN SECTION		UDEC INPUT PROPERTIES						
SURCHARGE LOADING B		INTACT ROCK PROPERTIES (Mohr-C		2.0880e+005 (lbf/ft ²)	SHEAR ZONE PRO	PERTIES (Mohr-Co	uimb Model):	
P- 1698 kips 8.3' 4 4 4 4 4 4 4 4 4 4 4 4 4	Density = 5.4390e (slug/ft ²) Youngs Modulus = 8.6400e+008 (lbt/ft ² Polisions Ratio = 2.5000e-001	(mt ²) Cohesion = 6.0e+003 Angle of friction = 50 Tensile Strength =5.0	Young's Modulus = 3.0e+008 (lbf/ft2) Cohesion = 6.0e+003 (lbf/ft2) Angle of fridom = 50" Tensile Strength =5.03e+003 (lbf/ft2) Polssons Ratio = 2.5000e-001					
40 deg 30' Rock Cover	30' Rock Cover	IN-SITU STRESS K ₉ = 2 Surcharge = See Column Loads on De	esign Section		OUNDWATER vater loads considered			
	JOINT PROPERTIERS (Mohr-Coulor	mb Model): Joint P	attern A					
		Joint Set	1 (Foliation)	2 (Cross - Foliation)	3(Conjugate)	4 (Random Low)	4 High	
	1 mil	True/ Apparent Dip (S.D)	40/40 (5)	60/ 65 (5)	50/45 (5)	NA	NA	
	V V V	Dip Direction (S.D.) Baseline Dip (GIR)	270 (5) 35	150 (5) 85	90 (5) 35	NA NA	NA NA	
		Baseline DD (GIR)	250	190	75	NA	NA	
		Mean Angle (S.D.) degrees						
		Mean Trace (S.D.) feet	50 (5)	25 (5)	50 (5)	NA	NA	
i mar i	- mar	Mean Gap (S.D.) feet	30 (5) 10 (2.5)	10 (2.5)	30 (5) 10 (2.5)	NA	NA NA	
		Mean Spacing (S.D.) feet Normal Stiffness (Ibf/tt ² /tt)	16000000	20 (2.5) 160000000	10 (2.5)	NA NA	NA	
		Shear Stiffness (Ibf/ft ² /ft)	8300000	8300000	8300000	NA	NA	
		Tensile Strength (lbf/ft ²)	0	0	0	NA	NA	
	KII	Friction Angle (degrees) øb	35	35	45	NA	NA	
		Dilation Angle (degrees) Ø	5	5	5	NA	NA	
		Cohesion (Ibfift ²)		0	0	NA	NA	
		CONSTRUCTION SEQUENCE : 3 TO			Stage Description			
		WEST CAVERN EAST CAVERN			1 TBM Tunnels excavated under contract CM009			
			5 6		2 Excavate West Cavern top heading - Install bolts 3 Excavate West Cavern top heading - Install bolts			
		2 3						
			Y 1	7 1		avern pillar - Install bi avern top heading - in		
			- K 2	X . A		avern top heading - in avern top heading - in		
ROCKBOLT SUMMARY - Final Stage West Cavern (Ib)	MOVEMENT SUMMARY - Top of Rock Subsidence at Final Excavation Stage (ft)	9		10	7 Excavate East C	avern pillar - install bo		
JOB TITLE : Excerv. strage 12 (of 12) Factored patiel avial force (FS+1.87)	JOB TITLE : Excerv.stage 12 (of 12) Y disp. upper surface model (TOR)		1		8 Excavate final tw			
UDEC (Version 4.00) (9405) 1.01 3 20 20	C(Varsion 4.00) 1/4 > > (r/c) 1/4 3 > > > (r/c) (r/c) <t< td=""><td>12 1</td><td colspan="3">9 Excavate two bench levels - install boits 10 Excavate two bench levels - install boits</td></t<>			12 1	9 Excavate two bench levels - install boits 10 Excavate two bench levels - install boits			
LEGEND 1.4	<u>15300</u>	8 11 1		-		nch levels - install bolt bench - install bolts	ts	
23-Mar-03 23:25 evela 1229010	23-War-03 2328 4.00			and a second second		ench - Install bolts		
Sine = 3.4625+01 sec 1.39 - table plot	cycle 1229910 Time - 3.4828+01 sec					and a solar bond		
View 0475 #1000000000000000000000000000000000000	Y 466, (f)00000000000 .1.00 -	NB. Top heading excavation in West Cavern to be kept 60' ahead of East Cavern top heading excavation						
HBOLT_A_ARO_L-RB-0875-#10co % mboLT_A_ARO_L-RB-0875-#10co bai HBOLT_A_ARO_L-RB-0875-#10co bai HBOLT_A_ARO_L-RB-0875-#10co bai	-1.522+02+07 values 1.522+02							
RECUT_A_BEN_1_L-SWAMA-24CDD	200 -							
RECUT A BEN J. ROWANI A todo RECUT A BEN J. ROWANI A todo zvo line tito control to book a saga		SUPPORT PROPERTIES	Crown/Arch	Sidewall		Crown/ Arch	Sidewall	
Vz. 1.00E+00+X values=1.50E+01 BH - 384	250 -	Bolt Type		SW-PM-24	Max compressive force (lbf)		4.50E+04	
2.00 × 10.00 ×		Bolt Length (ft)	15'	15'	Max tensile force (lbf)		4.50E+04	
schraddiller" http://www.internet.com/	4000 -	Spacing (ft) Radial / Longitudinal Cross sect. area (ft2)	5' x 5' 8.82E-03	5' x 5' 5.18E-03	Youngs modulus (lbf/ft2) Grout Stiffness (lbf/ft2)		4.18E+09 1.60E+09	
D.08		Diameter (ft)	1.1E-01	8.1E-02	Grouth Bond strength(lbf/ft)		7.00E+03	
-0.23	250	Pre-tension force (lbf)	3.00E+04	0				
0.00 0.20 0.50 0.50 0.00 1.00 1.20 1.40 1.50								
Orand Centrel Station 0.00 #.28 D/48 D/58 0.00 1.00 1.20 1.48 1.58	Grand Carthal Station -3.20 -1.00 -1.00 -0.00 0.50 1.00 1.50 2.00	Density (slug/ft3)	1.51E+01	1.51E+01				

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Excavation Sequence & Constructability challenges

headers have been developed

• Running tunnels already excavated through Caverns by TBM for speed of initial phase of construction

 Now adds challenge for identifying best sequence as the bores create an unconventional geometry and at 22' (6.7m) constrain the size of equipment.





Excavation sequences for both drill & blast or Road



Questions?



